



CAT I Examination – Winter Semester 2023-24

B.Tech – Chemical Engineering

Course: BCHE204L – Transport Phenomena

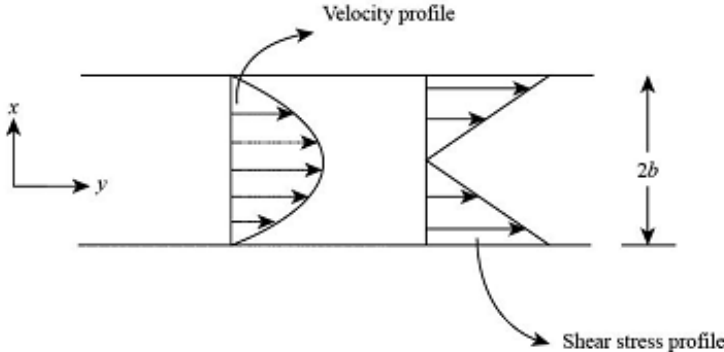
Time: 90 min

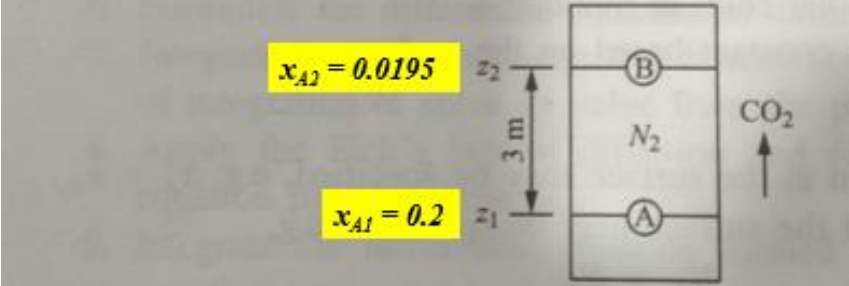
Slot: A2+TA2+TAA2

Max. Marks: 50

ANSWER KEY

1 (a)	Explain the analogy between momentum and energy transport in terms of relation between their fluxes and gradients, diffusivities and relation between their boundary layer thicknesses. (4M)												
Solution	<table><tr><th>Type of transport</th><th>Flux</th><th>Driving force</th><th>Equation</th></tr><tr><td>Momentum</td><td>Momentum flux</td><td>Velocity gradient</td><td>$\tau_{yx} = -\mu \frac{dv}{dy}$</td></tr><tr><td>Energy transport</td><td>Heat flux</td><td>Temperature gradient</td><td>$q_x = -k \frac{dT}{dy}$</td></tr></table> Prandtl number: $Pr = \frac{\nu}{\alpha} = \frac{\text{Momentum diffusivity}}{\text{Thermal diffusivity}}$ $\delta/\delta_t = (Pr)^{1/3}$ If the $Pr = 1$, then the hydrodynamic and thermal boundary layers are identical. If $Pr > 1$, then $\delta > \delta_t$. If $Pr < 1$, then $\delta < \delta_t$.	Type of transport	Flux	Driving force	Equation	Momentum	Momentum flux	Velocity gradient	$\tau_{yx} = -\mu \frac{dv}{dy}$	Energy transport	Heat flux	Temperature gradient	$q_x = -k \frac{dT}{dy}$
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1 (b)	Determine the heat loss per m^2 from a 40 cm thick furnace wall whose either side surface temperature are maintained at 50 °C and 300 °C. The thermal conductivity of material is given by $K = 0.005T - (5 \times 10^{-6}) T^2$ (T is in °C). (6M)
Solution	$q_x = -k \frac{dT}{dx}$ $q_x dx = -k dT$ $\int_0^L q_x dx = - \int_{50}^{300} k dT$ $q_x = -\frac{1}{L} \int_{50}^{300} (0.005T - 5 \times 10^{-6} T^2) dT$ $q_x = -\frac{1}{0.4} \left(0.005 \frac{T^2}{2} - \frac{5 \times 10^{-6}}{3} T^3 \right) \Big _{50}^{300} = 435 \text{ W/m}^2$
2 (a)	Draw the shear stress and velocity distribution for the flow of a fluid in a circular conduit under laminar flow condition. (4M)
Solution	
2 (b)	Water at 24 °C is filled between two parallel plates at some distance apart. The lower plate is being pulled at a constant velocity of 0.4 m/s faster relative to the top plate. The viscosity of water at 24 °C is 0.9142×10^{-3} kg/m.s. How far apart (cm) should the two plates be placed so that the shear stress is 0.3 N/m ² ? Also, calculate the shear rate. (6M)
Solution	Let Δy be the distance between the two plates. Shear stress, $\tau_{yx} = 0.3 \text{ N/m}^2$ Applying the Newton's law of viscosity, $\tau_{yx} = -\mu \frac{dv_x}{dy}$ or $\tau_{yx} \int_0^{\Delta y} dy = -\mu \int_{0.4v_x}^0 dv_x$ or $\tau_{yx} = \mu \frac{v_x}{\Delta y}$

	or $0.3 = \frac{0.9142 \times 10^{-3} \times 0.4}{\Delta y}$ $\therefore \Delta y = 0.9142 \times 10^{-3} \times \frac{0.4}{0.3} = 0.00122 \text{ m}$ $= 0.122 \text{ cm}$ Thus, shear rate, $\frac{\Delta v_x}{\Delta y} = \frac{0.4}{0.00122} = 327.8 \text{ s}^{-1}$
3	Carbon dioxide gas is diffusing through nitrogen gas in one direction at atmospheric pressure and temperature of 15 °C. The mole fraction of CO₂ at point A is 0.2 and at point B (3 m away in the direction of diffusion) is 0.0195. The concentration gradient is constant over this distance and diffusivity is $1.5 \times 10^{-5} \text{ m}^2/\text{s}$. The gas phase as a whole is stationary, i.e. N₂ is diffusing at the same rate as CO₂, but in opposite direction. (a) What is the molar flux of CO₂ in kmol/m².s? (5M) (b) What is the molar flux of N₂ in kmol/m².s? (5M)
Solution	Let A be the CO₂ species and B be the N₂ species. $\mathcal{D}_{AB} = 1.5 \times 10^{-5} \text{ m}^2/\text{s}$  Total pressure = 1 atm = $1.0132 \times 10^5 \text{ Pa}$ Temperature, $T = 15 \text{ }^\circ\text{C} = 273.1 + 15 = 288.2 \text{ K}$ $z_2 - z_1 = 3 \text{ m}$

Fick's law:

$$J_{Az}^* = -c \mathcal{D}_{AB} \frac{dx_A}{dz} \quad (i)$$

where c = concentration of the CO_2 - N_2 system.

or $c = \frac{P}{RT}$.

Now the molar flux of A becomes

$$J_{Az}^* = -\frac{P}{RT} \mathcal{D}_{AB} \frac{dx_A}{dz} \quad (ii)$$

where x_A = mole fraction of A.

Integrating Eq. (ii), we have

$$J_{Az}^* \int_{z_1}^{z_2} dz = -\frac{P}{RT} \mathcal{D}_{AB} \int_{x_{A1}}^{x_{A2}} dx \quad (iii)$$

or $J_{Az}^* (z_2 - z_1) = \frac{P}{RT} \mathcal{D}_{AB} (x_{A1} - x_{A2})$

or $J_{Az}^* = \frac{P}{RT} \mathcal{D}_{AB} \left(\frac{x_{A1} - x_{A2}}{z_2 - z_1} \right) \quad (iv)$

Substituting the above values in Eq. (iv), we get

$$J_{Az}^* = \frac{1.0132 \times 10^5 \times 1.5 \times 10^{-5}}{8314 \times 288.1} \left(\frac{0.2 - 0.0195}{3.0 - 0} \right)$$
$$= 0.38 \times 10^{-7} \text{ kg mol of A/m}^2 \cdot \text{s} \quad \text{Ans. (a)}$$

For the component B, i.e. N_2 ,

mole fraction of B, $x_{B1} = 1 - 0.2 = 0.8$

mole fraction of B, $x_{B2} = 1 - 0.0195 = 0.9805$

$$x_{A1} + x_{B1} = 1.0$$

The mole flux for B, J_{Bz}^* , can be written as

$$J_{Bz}^* = \frac{P \mathcal{D}_{BA}}{RT} \left(\frac{x_{B1} - x_{B2}}{z_2 - z_1} \right) \quad (v)$$

Substituting the values in Eq. (v), we get

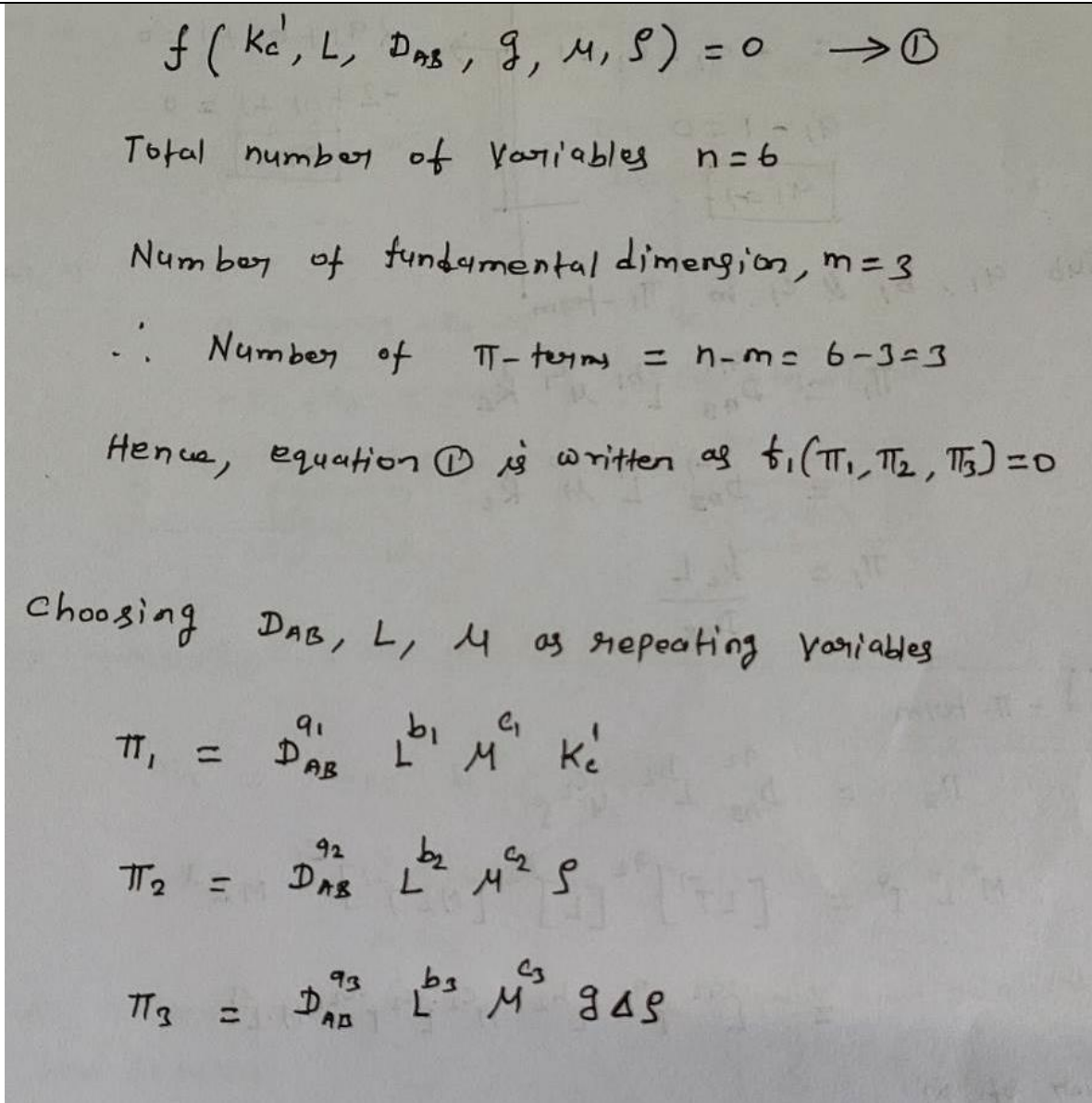
$$J_{Bz}^* = \frac{1.0132 \times 10^5 \times 1.5 \times 10^{-5} (0.8 - 0.9805)}{8314 \times 288.1 (3.0 - 0)}$$
$$= -0.38 \times 10^{-7} \text{ kmol of B/m}^2 \cdot \text{s} \quad \text{Ans. (b)}$$

Note: For an ideal gas, $\mathcal{D}_{AB} = \mathcal{D}_{BA}$

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The mass flux from a 5 cm diameter naphthalene ball placed in stagnant air at 40°C and atmospheric pressure is $1.47 \times 10^{-3} \text{ mol/m}^2 \cdot \text{s}$. Assume the vapour pressure of naphthalene to be 0.15 atm at 40°C and negligible bulk concentration of naphthalene in air. If air starts blowing across the surface of naphthalene ball at 3 m/s, by what factor will the mass transfer rate increase, all other conditions remaining the same?

	For spheres: $Sh = 2.0 + 0.6 (Re)^{0.5} (Sc)^{0.33}$ Where, Sh is the Sherwood number and Sc is the Schmidt number. The viscosity and density of air are $1.8 \times 10^{-5} \text{ kg/m.s}$ and 1.123 kg/m^3, respectively and the gas constant is $82.06 \text{ cm}^3\text{atm/mol.K}$.
Solution	$Sh = \frac{k_c L}{D_{AB}}$ where L is the characteristic dimension for sphere L = Diameter. $Sc = \frac{\mu}{\rho D_{AB}}$ $Re = \frac{D v \rho}{\mu}$ Mass flux, $N_A = K_c \Delta c$ -----(1) $Sh = 2.0 + 0.6 (Re)^{0.5} (Sc)^{0.33}$ $\frac{k_c D}{D_{AB}} = 2.0 + 0.6 \left[\frac{D v \rho}{\mu} \right]^{0.5} \left[\frac{\mu}{\rho D_{AB}} \right]^{0.33}$ ----- (2) also $N = K_G \Delta \bar{p}_A$ $K_G = \frac{k_c}{RT}$ Given: $N = 1.47 \times 10^{-3} \frac{\text{mol}}{\text{m}^2 \cdot \text{sec}} = \frac{K_c}{RT} \Delta \bar{p}_A$ $\frac{k_c}{RT} \left[\frac{0.15}{1} - 0 \right] = 1.47 \times 10^{-3} \times 10^{-4} \frac{\text{mol}}{\text{cm}^2 \cdot \text{sec}}$ $k_c = \frac{1.47 \times 10^{-7}}{0.15} \times 82.06 \times (273 + 40)$ $= 0.0252 \text{ cm/sec}$ $k_c = 2.517 \times 10^{-4} \text{ m/sec}$ -----(3) Estimation of D_{AB}: From (2), $\frac{2.517 \times 10^{-4} \times 5 \times 10^{-2}}{D_{AB}} = 2 \text{ (since } v = 0)$ Therefore $D_{AB} = 6.2925 \times 10^{-6} \text{ m}^2/\text{sec}$. $\frac{k_c \times 5 \times 10^{-2}}{6.2925 \times 10^{-6}} = 2 + 0.6 \left[\frac{5 \times 10^{-2} \times 3 \times 1.123}{1.8 \times 10^{-5}} \right]^{0.5} \left[\frac{1.8 \times 10^{-5}}{1.123 \times 6.2925 \times 10^{-6}} \right]^{0.33}$ $7946 k_c = 2 + 0.6 \times (96.74) \times (1.361)$ $k_c = 0.0102 \text{ m/sec}$. ----- (4)

	$\frac{(4)}{(3)} = \frac{N_{A2}}{N_{A1}} = \frac{0.0102}{2.517 \times 10^{-4}} = 40.5$ Therefore, rate of mass transfer increases by 40.5 times the initial conditions.
5	Using Buckingham's π-theorem, show that Sherwood Number (Sh) is a function of Grashoff (Gr) and Schmidt (Sc) number for free convection mass transfer. Sh = f (Gr, Sc) The dimensionless groups can be formulated using mass transfer coefficient k'_c (LT^{-1}) and other variables such as L, ρ, μ, D_{AB}, g and $\Delta\rho$ where L is the pipe length, $\Delta\rho$ is the density difference, μ is the viscosity of the fluid and D_{AB} is the diffusivity of the fluid.
Solution	 Handwritten solution for the problem using Buckingham's π-theorem: $f(k'_c, L, D_{AB}, g, \mu, \rho) = 0 \rightarrow \text{①}$ Total number of variables $n = 6$ Number of fundamental dimension, $m = 3$ $\therefore$ Number of π-terms = $n - m = 6 - 3 = 3$ Hence, equation ① is written as $f_1(\pi_1, \pi_2, \pi_3) = 0$ Choosing D_{AB}, L, μ as repeating variables $\pi_1 = D_{AB}^{a_1} L^{b_1} \mu^{c_1} k'_c$ $\pi_2 = D_{AB}^{a_2} L^{b_2} \mu^{c_2} \rho$ $\pi_3 = D_{AB}^{a_3} L^{b_3} \mu^{c_3} g \Delta\rho$

First - π -term

$$M^0 L^0 T^0 = (L^2 T^{-1})^{a_1} L^{b_1} (M L^{-1} T^{-1})^{c_1} L^1 T^{-1}$$

Equating power of M

$$\begin{aligned} & \downarrow \\ & 0 = c_1 \\ & c_1 = 0 \end{aligned}$$

Equating powers of L

$$0 = 2a_1 + b_1 - c_1 + 1$$

$$2a_1 + b_1 + 1 = 0 \quad [\because c_1 = 0]$$

Equating power of T

$$0 = -a_1 - c_1 - 1$$

$$a_1 - 1 = 0$$

$$\boxed{a_1 = 1}$$

$$2a_1 + b_1 + 1 = 0$$

$$-2 + b_1 + 1 = 0$$

$$\boxed{b_1 = 1}$$

Sub a_1 , b_1 & c_1 in π_1 -term.

$$\pi_1 = D_{AB}^{a_1} L^{b_1} \mu^{c_1} k_c$$

$$= D_{AB}^{-1} L^1 \mu^0 k_c$$

$$\pi_1 = \frac{k_c L}{D_{AB}}$$

Second π -term

$$\begin{aligned}\pi_2 &= D_{AB}^{a_2} L^{b_2} \mu^{c_2} S \\ M^0 L^0 T^0 &= [L T^{-1}]^{a_2} [L]^{b_2} [M L^{-1} T^{-1}]^{c_2} M L^{-3} \\ &= L^{2a_2 - a_2} T^{-a_2} L^{b_2} M^{c_2} L^{-c_2} T^{-c_2} M L^{-3}\end{aligned}$$

powers of M

$$0 = c_2 + 1$$

$$\boxed{c_2 = -1}$$

power of L

$$0 = 2a_2 + b_2 - c_2 - 3$$

$$2a_2 + b_2 - c_2 - 3 = 0$$

$$2a_2 + b_2 + 1 - 3 = 0 \quad [\because c_2 = -1]$$

$$2a_2 + b_2 - 2 = 0$$

Power of T

$$0 = -a_2 - c_2$$

$$a_2 - c_2 = 0$$

$$\therefore a_2 = -c_2 \Rightarrow \boxed{a_2 = 1}$$

$$2a_2 + b_2 - 2 = 0$$

$$2 + b_2 - 2 = 0$$

$$\boxed{b_2 = 0}$$

$$\begin{aligned}\pi_2 &= D_{AB}^{a_2} L^{b_2} \mu^{c_2} S \\ &= D_{AB}^1 L^0 \mu^{-1} S \\ &= \frac{S D_{AB}}{\mu}\end{aligned}$$

Third - π term

$$\pi_3 = D_{AB}^{a_3} L^{b_3} \mu^{c_3} g \Delta T$$

$$M^0 L^0 T^0 = [L^2 T^{-1}]^{a_3} [L]^{b_3} [M L^{-1} T^{-1}]^{c_3} M L^{-2} T^{-2}$$

$$= L^{2a_3 - a_3} T^{-a_3} L^{b_3} M^{c_3} L^{-c_3} T^{-c_3} M^1 L^{-2} T^{-2}$$

power of M

$$0 = c_3 + 1$$

$$\rightarrow \boxed{c_3 = -1}$$

power of L

$$0 = 2a_3 + b_3 - c_3 - 2$$

$$2a_3 + b_3 + 1 - 2 = 0$$

$$2a_3 + b_3 - 1 = 0$$

power of T

$$0 = -a_3 - c_3 - 2$$

$$-a_3 - c_3 - 2 = 0$$

$$-a_3 + 1 - 2 = 0$$

$$\boxed{a_3 = -1}$$

$$2(-1) + b_3 - 1 = 0$$

$$b_3 - 3 = 0$$

$$\boxed{b_3 = 3}$$

Sub. a_3, b_3 & c_3 in π_3 term.

$$\pi_3 = D_{AB}^{-1} L^3 \mu^{-1} g \Delta T$$

$$\pi_3 = \frac{L^3 g \Delta T}{\mu D_{AB}}$$

As all the π -terms are dimensionless, the following manipulations are possible.

$$\pi_1' = \pi_1 \times \pi_2$$

$$\pi_2' = \pi_2 \times \pi_3$$

$$\pi_3' = \pi_3 \times \pi_1$$

$$\pi_2' = \pi_2 \times \pi_3 = \frac{L^3 g \Delta T}{\mu \cancel{D_{AB}}} \times \frac{\cancel{D_{AB}}}{\mu}$$

$$= \frac{g L^3 \Delta T}{\mu^2}$$

Combining all the π terms;

$$\frac{k_c' L}{D_{AB}} = f \left[\frac{g L^3 \Delta T}{\mu^2}, \frac{\mu}{\rho D_{AB}} \right]$$

$$Sh = f(Gr, Sc)$$